

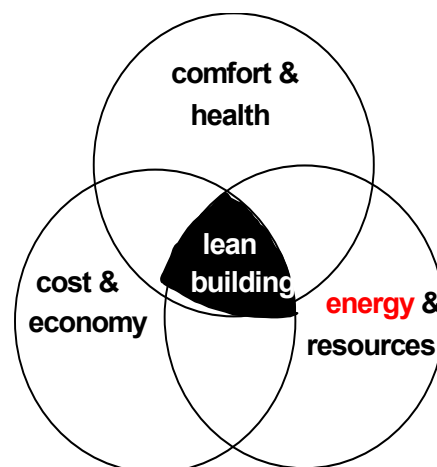
Energy efficiency in buildings and new technologies

Czech-Austrian Winter/Summer School

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Whole life
optimised
building

=>



Gebäudebestand in Österreich

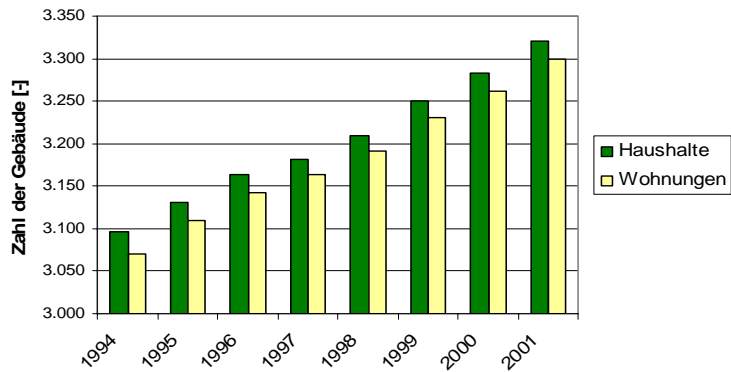
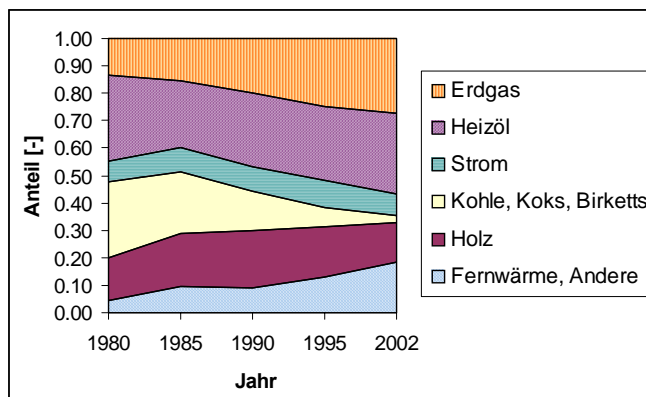


Abbildung: Entwicklung des Gebäudebestandes in Österreich, Quelle: www.statistik.austria.at, 15.03.2005

Quelle: Statistik Austria, (2004)

Energy carriers in Austrian households



Quelle: Statistik Austria, (2005)

Heating values and specific CO₂-emissions of fossil fuels

Energy carrier	Lower heating value	CO ₂ -emissions (related to lower heating value)
Hard coal	8,14 kWh/kg	0,350 kg/kWh
Lignite	2,68 kWh/kg	0,410 kg/kWh
Lignite briquetts	5,35 kWh/kg	0,380 kg/kWh
Coke	7,50 kWh/kg	0,420 kg/kWh
Heavy duty oil	10,61 kWh/l	0,290 kg/kWh
Oil „extra light“	10,08 kWh/l	0,270 kg/kWh
Natural gas	10,00 kWh/m ³	0,200 kg/kWh

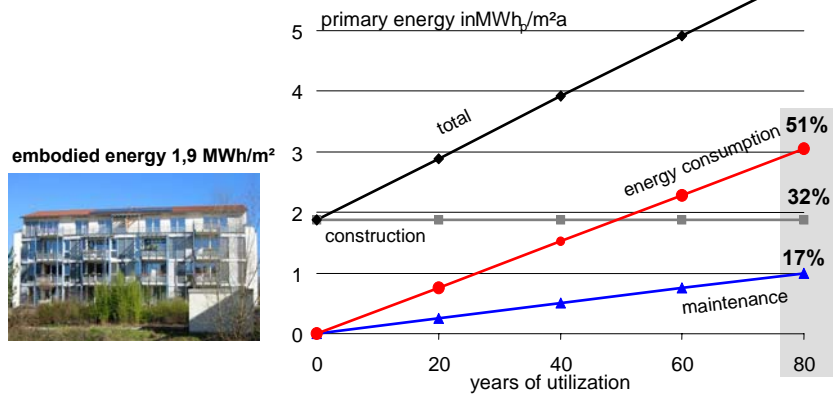
Energy balance of a building over its lifetime

Construction

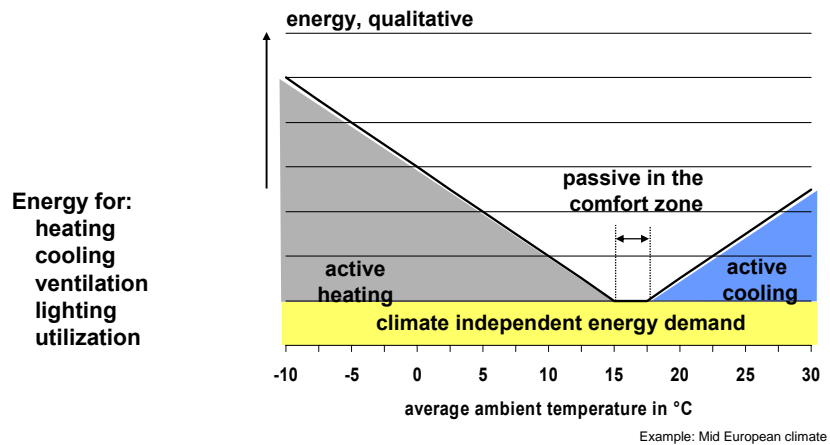
Maintenance

Energy consumption

Life Cycle Energy

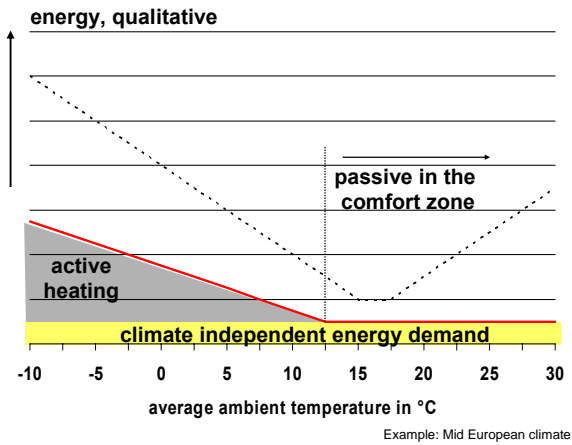


Current Buildings

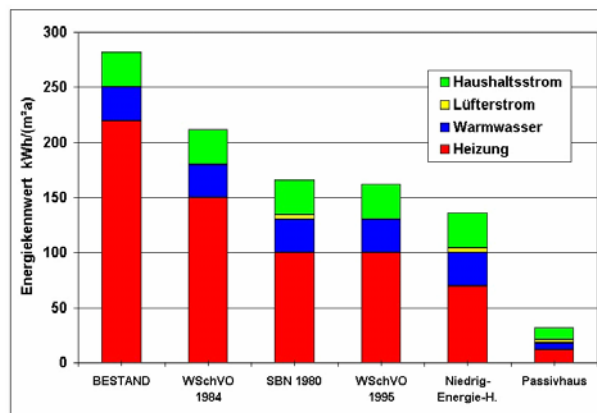


Lean Buildings

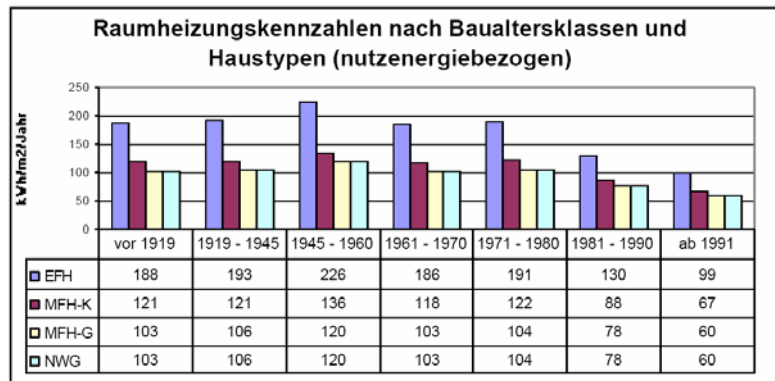
Energy for:
heating
cooling
ventilation
lighting
utilization



Energy demand of buildings

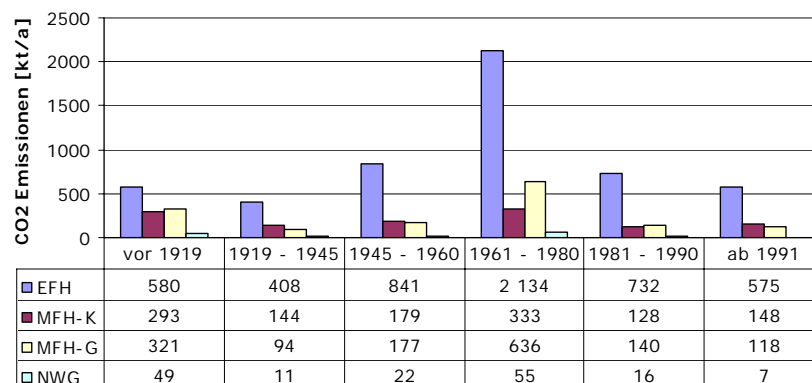


Specific space heating energy demand of single (SFH) and multi family buildings (MFH-K : small, MFH-G big) in dependenc of year of errection in Austria



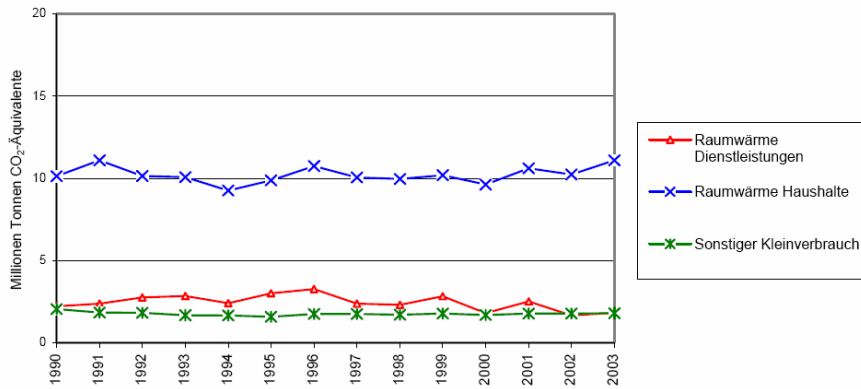
Quelle: Jungmeier, et al. (1996)

CO₂-emissions from space heating of appartements in Austria



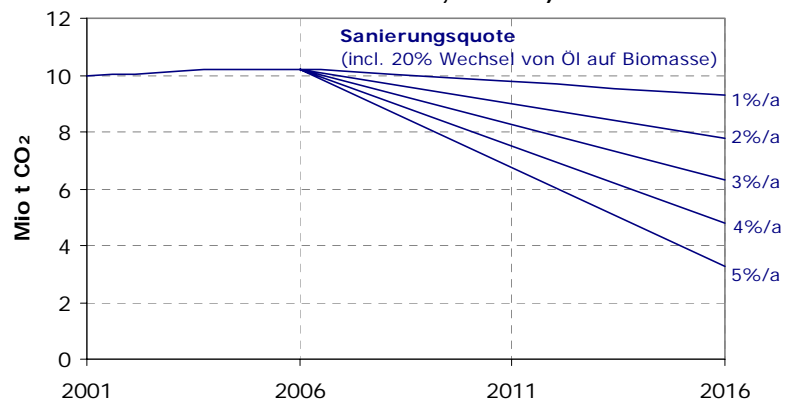
Quelle: eigene Berechnung

CO₂-equivalent emissions from the residential sector (Raumwärme Haushalte) and other small



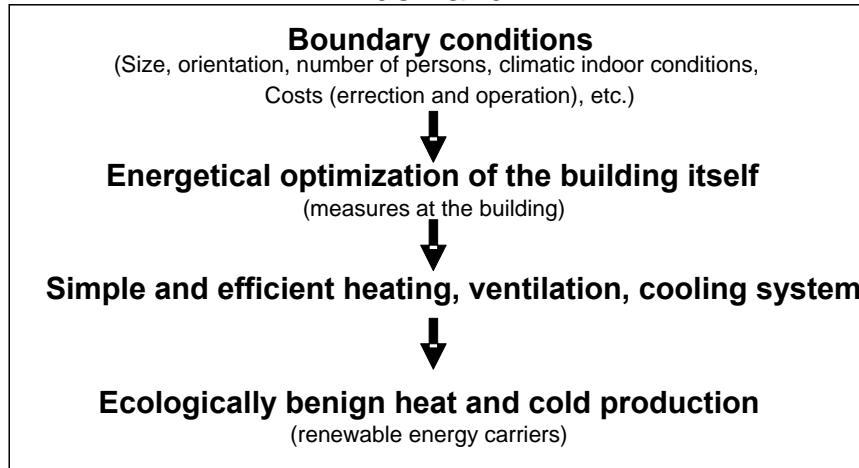
Quelle: BMLFUW (2005)

Trendscenario of thermal renovation and fuel switch of all Austrian dwellings (basic data from Statistik Austria, 2001)



Quelle: eigene Berechnung

Steps of integrated building design für low energy demand



Energetical System Building

Building behaviour

- Active thermal mass
- Passive solar energy use

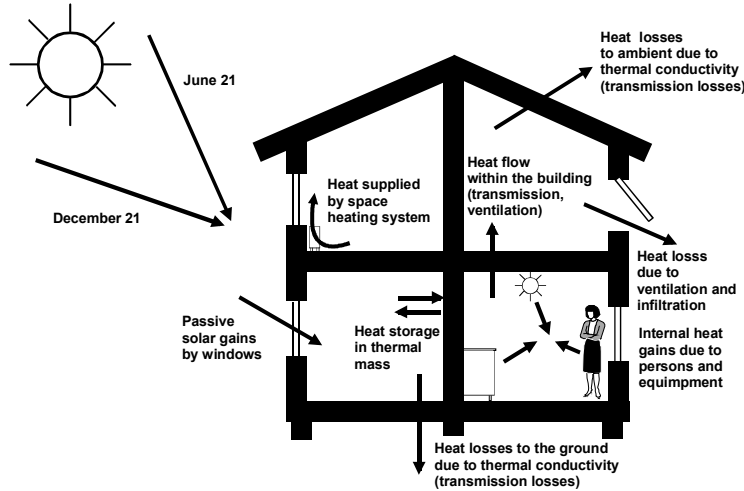
User behaviour

- Ventilation
- Internal Heat gains
- Indoor air set temperature
- Shading

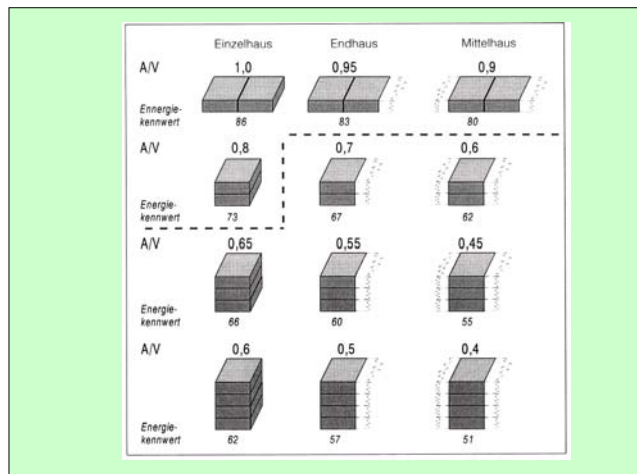
Control

- Indoor air temperature controlled (centralized, decentralized)
- Outdoor air temperature dependend (centralized)
- Analog - digital
- Irradiation controlled
- Positioning of sensors

Energetical System Building



Building Shape: Ratio of A/V for differetn shapes



Quelle: Feist, W., 1998, Das Niedrigenergiehaus

Heat transfer coefficient for transmission heat losses

$$U = \frac{\dot{Q}}{A \cdot \Delta T} (=k) \quad [\text{W}/(\text{m}^2\text{K})]$$

mit A... Heat transfer surface [m²]

\dot{Q} ... Transferred heat [W]

ΔT ... Forcing temperature difference [K]

$$\dot{q} = \frac{\dot{Q}}{A} = U \cdot \Delta T \quad \dots \text{specific heat flow } [\text{W}/\text{m}^2]$$

Heat conduction through a wall

$$\frac{1}{U} = \frac{1}{\alpha_i} + \sum_n \frac{s_n}{\lambda_n} + \frac{1}{\alpha_a}$$

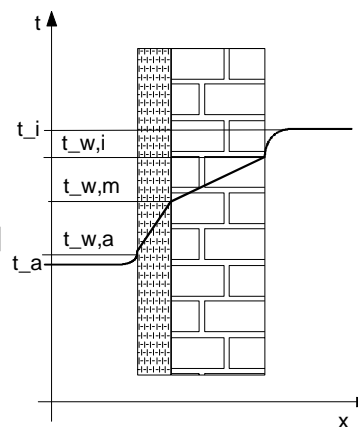
$$R = R_i + \sum_n R_n + R_a$$

mit α ... heat transfer coefficient [W/(m² K)]

λ_n ... thermal conductivity [W/(m K)]

s_n ... thickness of layer [m]

R ... thermal resistance [(m² K)/W]

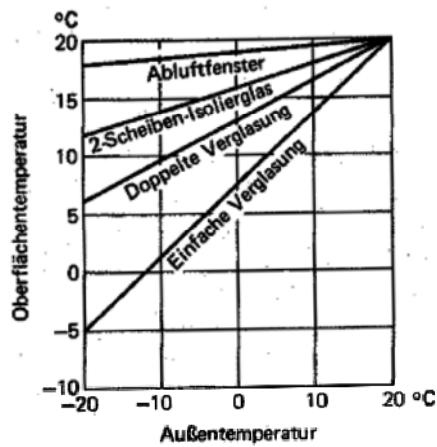
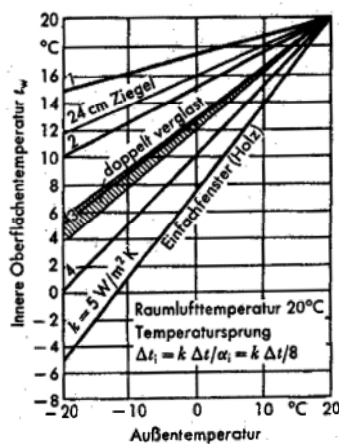


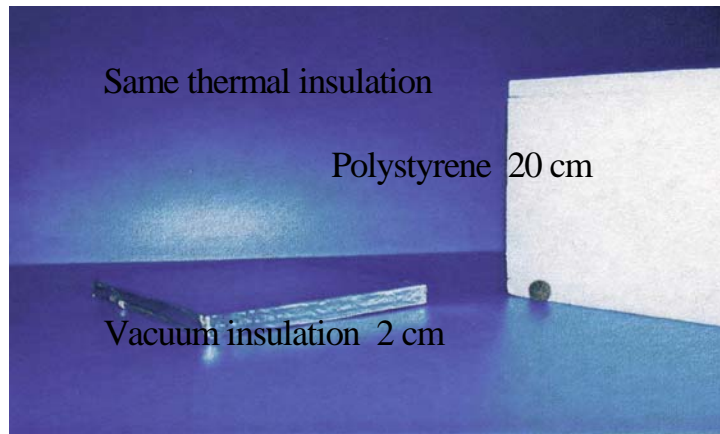
Maximum U-values (W/m²K) for Austrian provinces (2003)

Stand: 9/2003	B	K	N	O	S	St	T	V	W
gültig seit	'02	'97	'96	'99	'02	'97	'98	'96	'01
Außenwand	0,38	0,40	0,40	0,50	0,35	MFH: 0,50 EFH: 0,40	0,35	0,35	0,50
Wände gegen unbeheizte Gebäudeteile und Feuermauern	0,50	0,70	0,70	0,70	0,50	0,70	0,50	0,50	0,50
Wände gegen getrennte Wohn- und Betriebseinheiten	0,90	1,60	1,60	1,60	0,90	1,60	0,90	1,60	0,90
Decken gegen Außenluft, Dachböden, Durchfahrten	0,20	0,25	0,22	0,25	0,20	0,20	0,20	0,25	0,25
Decken gegen unbeheizte Gebäudeteile	0,35	0,40	0,40	0,45	0,40	0,40	0,40	0,40	0,45
Decken gegen getrennte Wohn- und Betriebseinheiten	0,70	0,90	0,90	0,90	0,90	0,90	0,70	0,90	0,90
Fenster	1,70	1,80	1,80	1,90	1,70	1,90	1,70	1,80	1,90
Außentüren	1,70	1,80	1,80	1,90	1,70	1,70 / 1,90	1,70	1,90	1,90
Erdberührte Wände	0,35	0,50	0,50	0,50	0,40	0,50	0,40	0,50	0,50
Erdberührte Fußböden	0,35	0,50	0,50	0,50	0,28 5	0,50	0,40	0,50	0,45

Abkürzungen:
MFH Mehrfam. Haus
EFH/ZFH ... Ein- u. Zweifam. Haus
GT Glastüre

Room air temperature – temperature of surrounding surfaces ⇔ thermal comfort

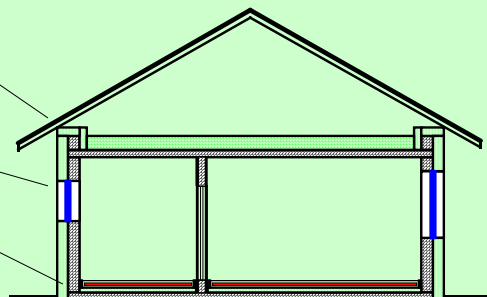




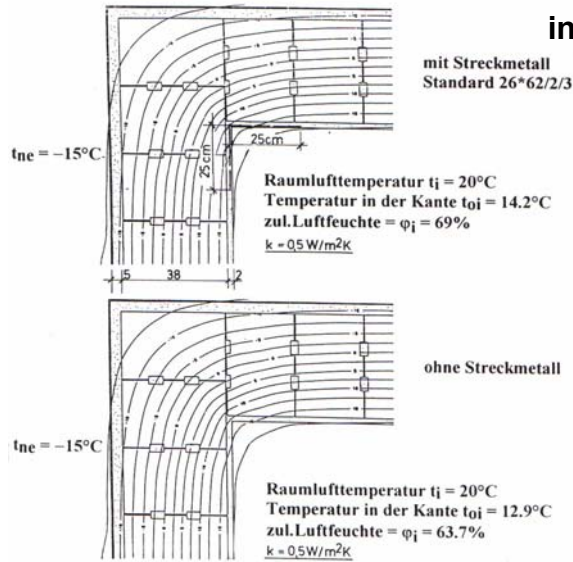
Avoiding thermal bridges

Problematic zones:

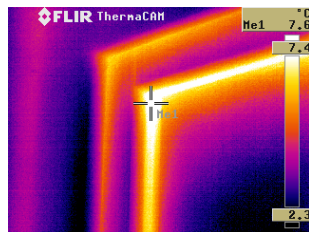
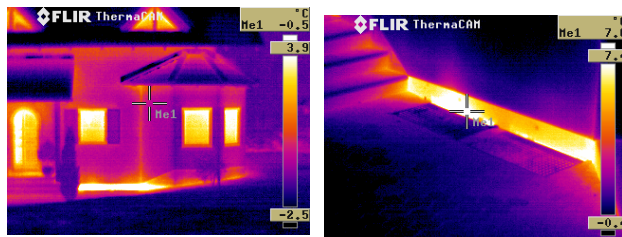
- Connection of roof
- Windows
- Floor e.g. cellar ceiling
- Balkonies



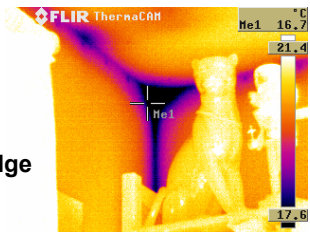
Course of temperature in an edge



Thermal bridges, Thermographie



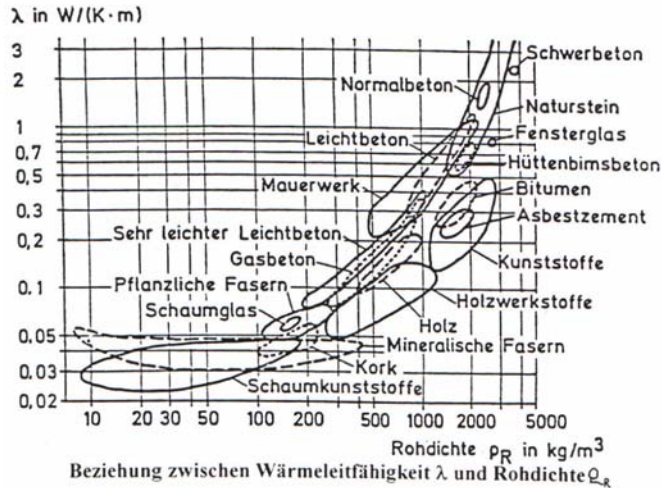
Ground floor to cellar,



Window

interior edge

Material: Thermal conductivity λ and density ρ



Principal of active thermal mass

$$\dot{q} = -\lambda \frac{\partial T}{\partial x} \quad \frac{\partial \dot{q}}{\partial x} = -\lambda \frac{\partial^2 T}{\partial x^2} = \rho_{sp} c_p \frac{\partial T}{\partial t}$$

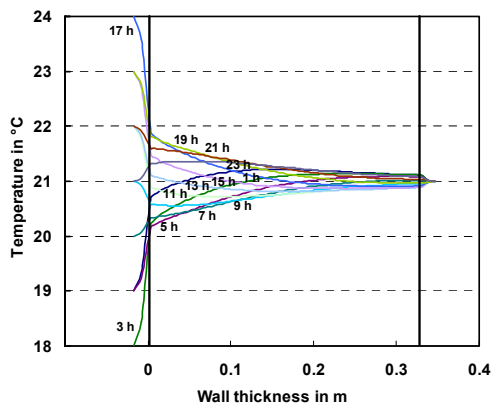
Needs room air temperature shifts

Stored and released heat :
0.076 kWh/(m² d).

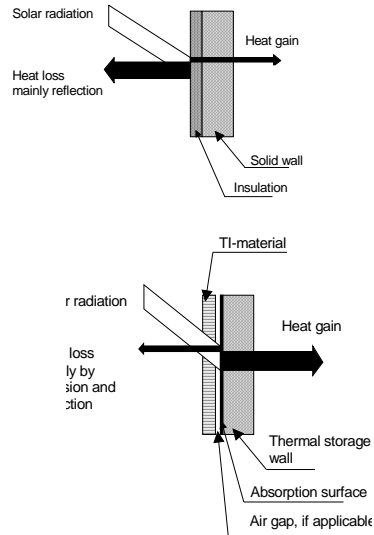
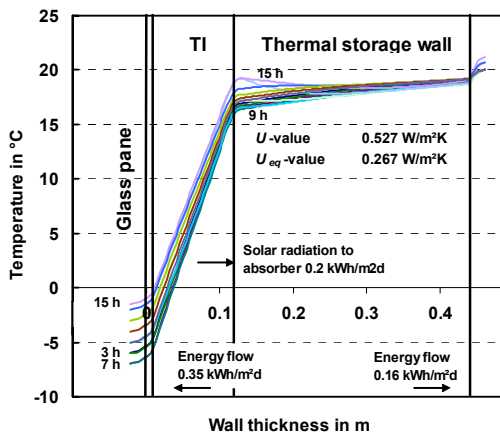
Significant temperature change up to a depth of ca. 10 cm (concrete wall)

It is not useful to make this wall thicker

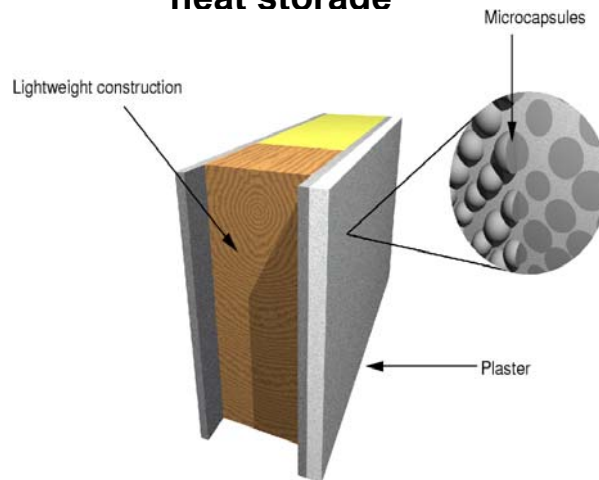
Thermal mass means AREA not DEPTH



Transparent Insulation

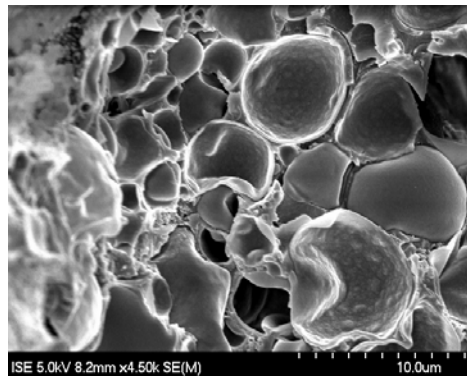


Micro-encapsulated phase change material, heat storage



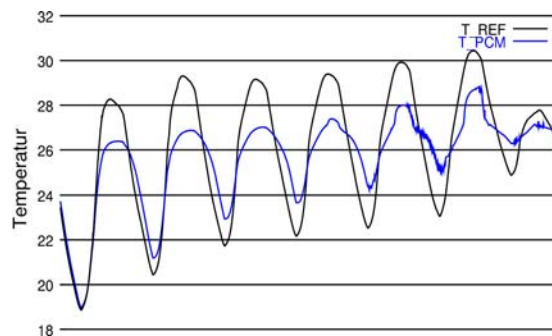
Micro encapsulated phase change materials

- Organic phase change materials
- PMMA-capsule (BASF), ~20 μm
- Integration into plaster, gipsum, concrete
- Increase of the thermal mass in a small temperature range
- Reduction of temperature peaks in summer time
- No active air conditioning



Application of PCMs on inner walls

Temperature behaviour of a test and a reference cell in comparison



Energy transmittance through windows

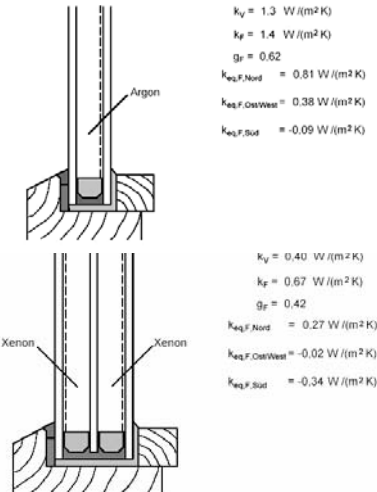
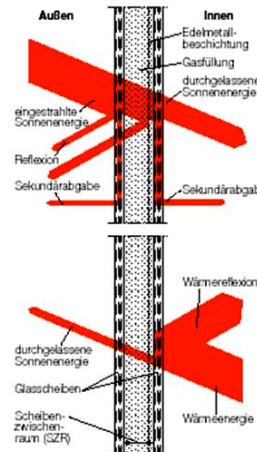


Bild 3.7: Wärmedurchgang durch ein Fenster mit Wärmeschutzglas (schematische Darstellung)



Energy transmittance (g) and heat transfer coefficient (U) for different glazings

	Diffuse g-value	U-value glazing in $\text{W/(m}^2\text{K)}$
Insulating glazing (4 + 16 + 4 mm, air)	0.65	3.00
Thermal insulation double-glazing (4 + 14 + 4 mm, argon)	0.60	1.30
Thermal insulation double-glazing (4 + 14 + 4 mm, xenon)	0.58	0.90
Thermal insulation triple-glazing with argon filling	0.44	0.80
Thermal insulation triple-glazing with krypton filling	0.44	0.70
Thermal insulation triple-glazing with xenon filling	0.42	0.40
10 cm plastic capillaries, one cover pane	0.67	0.90
10 cm plastic honeycombs, one cover pane	0.71	0.90
10 cm glass capillaries, two panes	0.65	0.97
2.4 cm granular aerogel, two panes filled with air	0.50	0.90
2 cm evacuated (100 mbar) aerogel plate, two panes	0.60	0.50

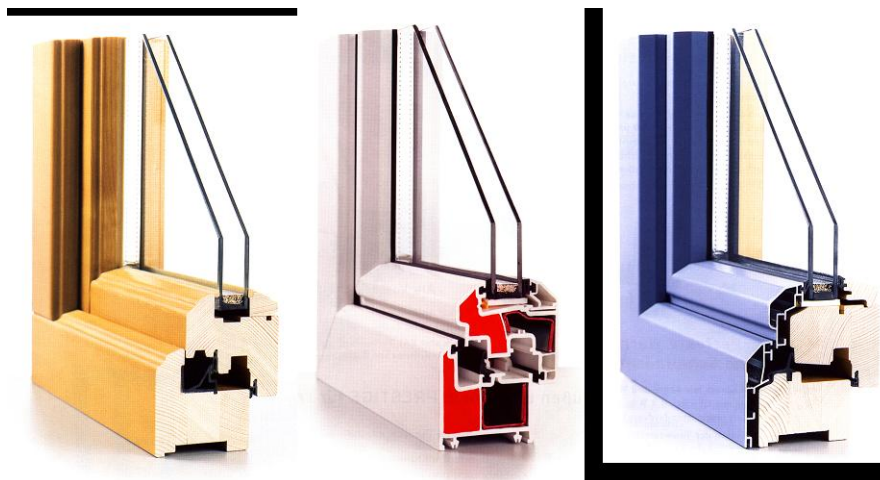
The diffuse g-values were measured for a poor in iron 4 mm front pane, whereas for the U-values an average sample temperature of 10 °C has been assumed.

$$U_{eq} = U_w - S_F g \quad S_F = 0,95 \text{ north, } 1,65 \text{ east/west, } 2,4 \text{ south}$$

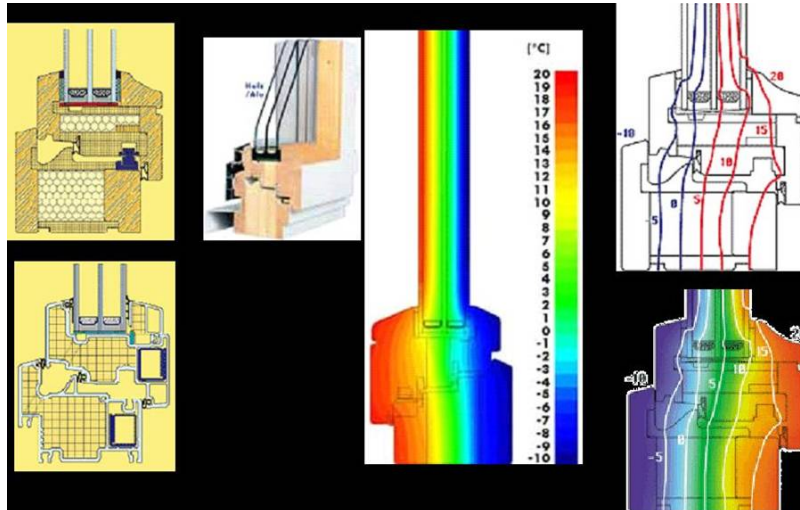
Diffuse g-value ($g_{diffuse}$), U-value of the window (U_w) and equivalent U-values (U_{eq}) corresponding to different glazing types (see /3-5/)

	$g_{diffuse}$	U_w	U_{eq} (south)	U_{eq} (east/west)	U_{eq} (north)
Simple glazing	0.87	5.8	3.7	4.4	5.0
Double-glazing (air 4 + 12 + 4 mm)	0.78	2.9	1.0	1.6	2.2
Double-glazing with thermal insulation and argon filling (6 + 15 + 6 mm)	0.60	1.5	0.1	0.5	0.9
Triple-glazing with thermal insulation and krypton filling (4 + 8 + 4 + 8 + 4 mm)	0.48	0.9	-0.3	0.1	0.4
Triple-glazing with thermal insulation and xenon filling (4 + 16 + 4 + 16 + 4 mm)	0.46	0.6	-0.5	-0.2	0.2

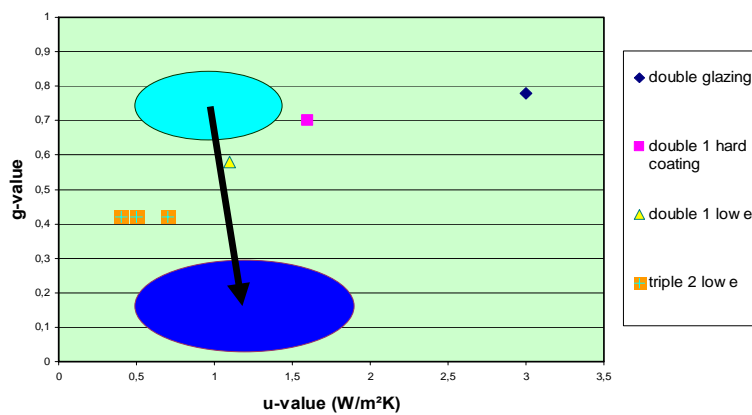
2-panes windows



3-pane low U windows



Potential for future glazings



Switchable glazings



Factors influencing the solar transmittance of windows

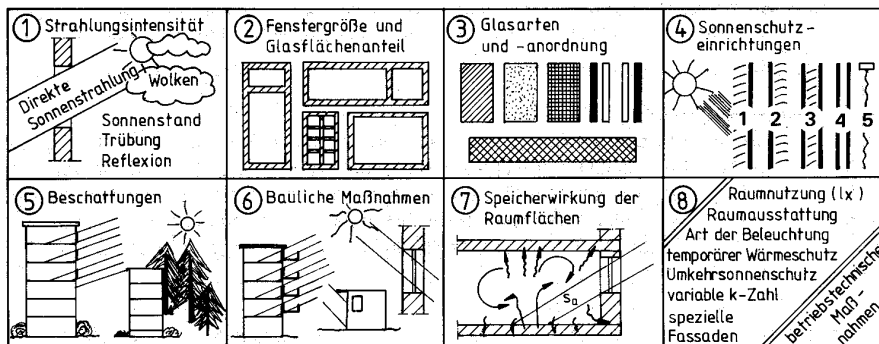
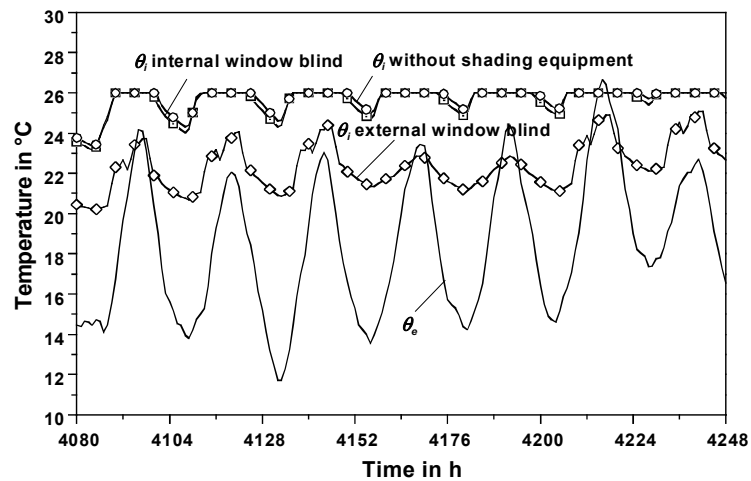


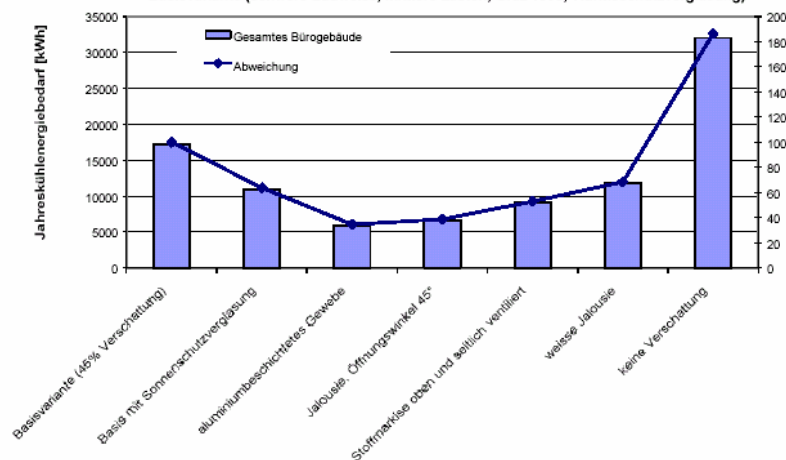
Abb. 7.24 Einflußgrößen auf Sonnenwärme durch Fenster

Shading by internal and external window blinds (θ_e ambient temperature, θ_i room temperature)

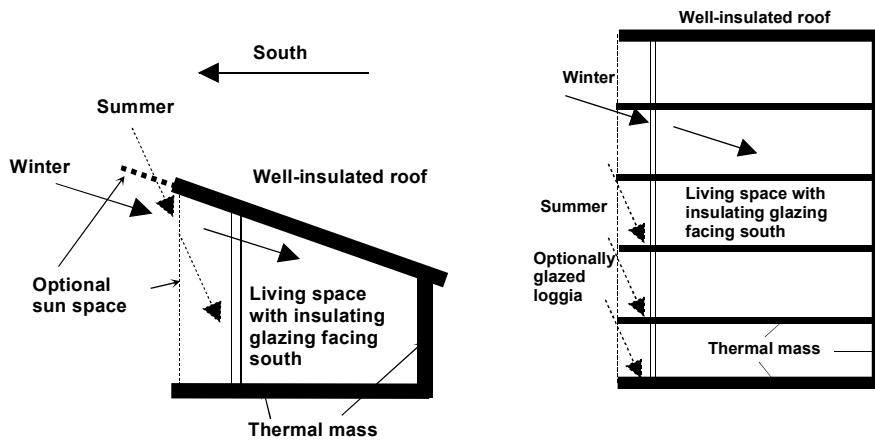


Cooling energy demand for different shading strategies in an office building

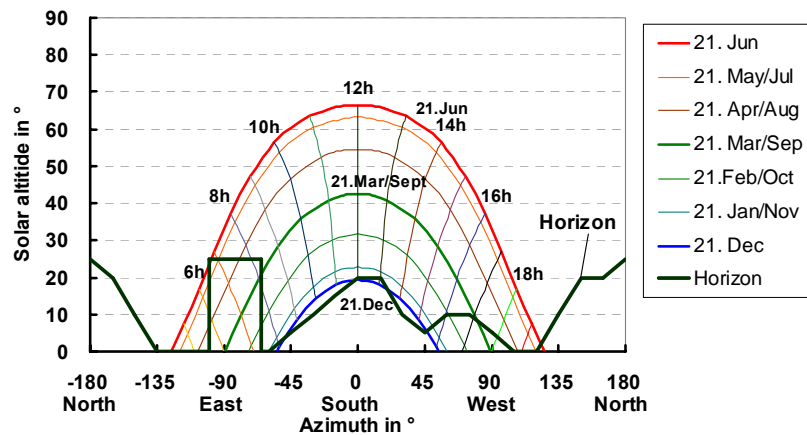
Änderung des Jahreskühlenergiebedarfs bei verschiedenen Verschattungsvarianten
Basisvariante (schwere Bauweise, mittlere Lasten; Graz 1998; Wärmeschutzverglasung)



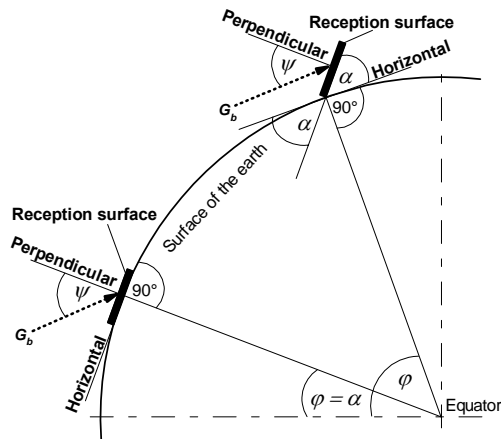
**Shading of transparent building surfaces by roof overhangs
(left: one family home, right: multiple families home)**



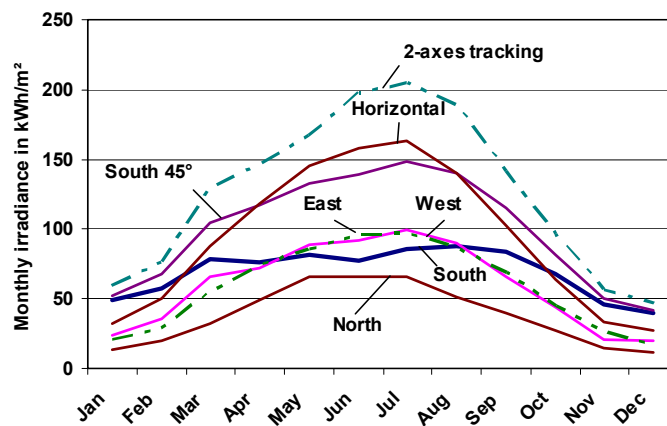
Solar position plot



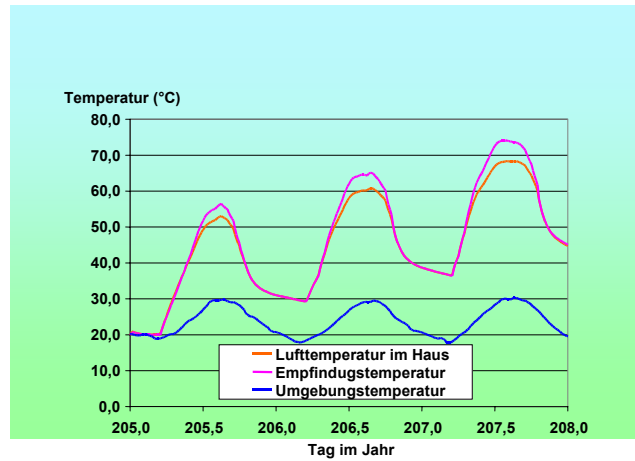
Geometrical interrelationship of solar radiation incident on tilted surfaces



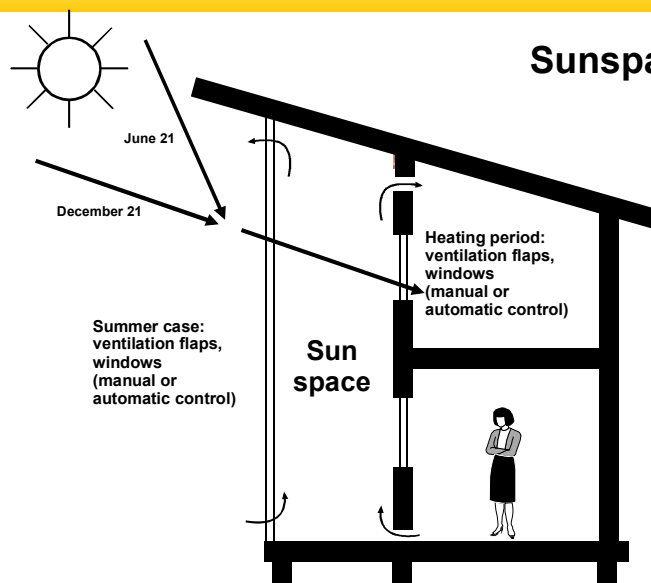
Global radiation incident on surfaces with various alignments in Central Europe (climate Graz/Austria, 47° latitude)



Summer Overheating in an office building (simulated)

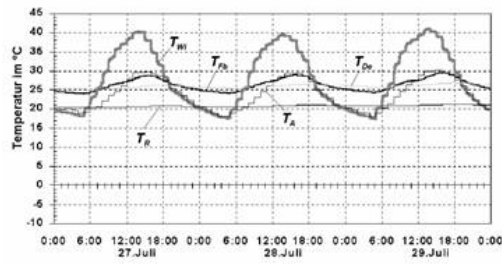


Sunspaces



Sunspace

TU Graz



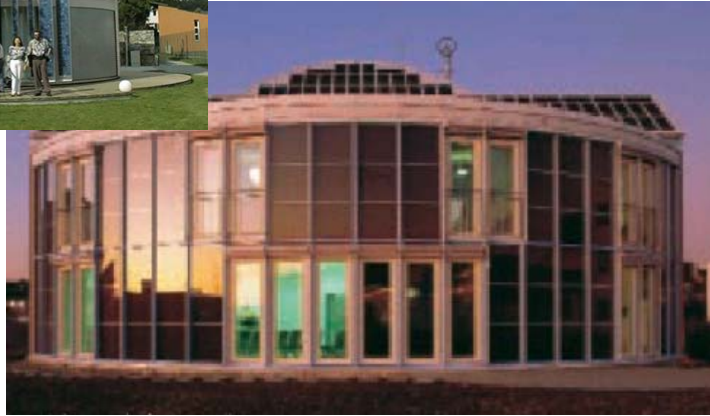
TU Graz

Low-energy lean multi family building





Solar houses

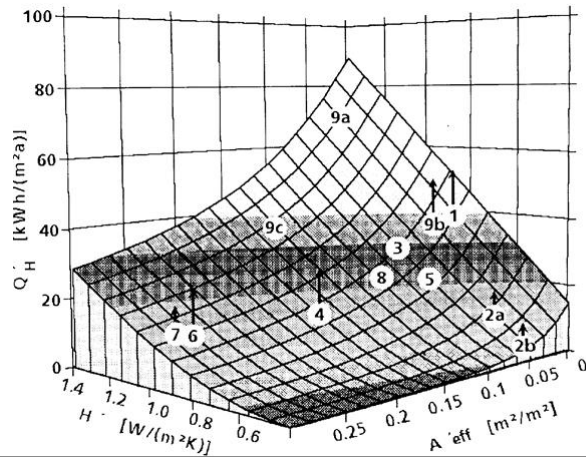


„Passive row houses“



„Solarhouses“ – „Passivhouses“

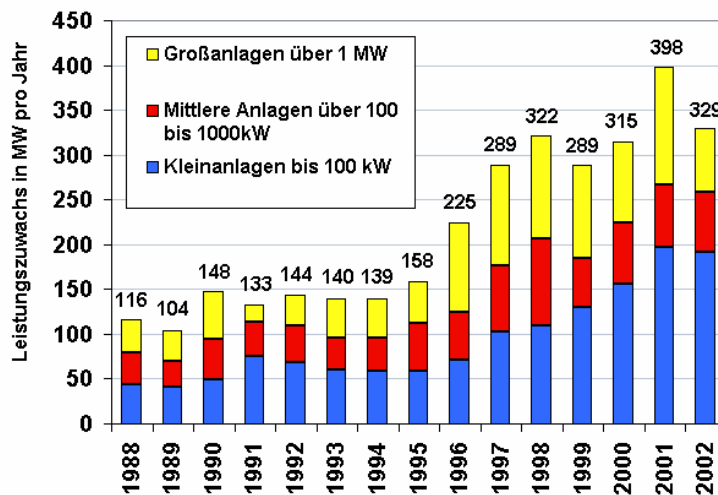
Gebäudekennfeld für ein Gebäude mittelschwerer Bauart und einigen realisierten Gebäuden: 7: Solarhaus Freiburg, 2: Passivhaus Kranichstein (a: Endhaus, b: Mittelhaus), Q'H: spezifischer Heizenergiebedarf (Voss, 1997)



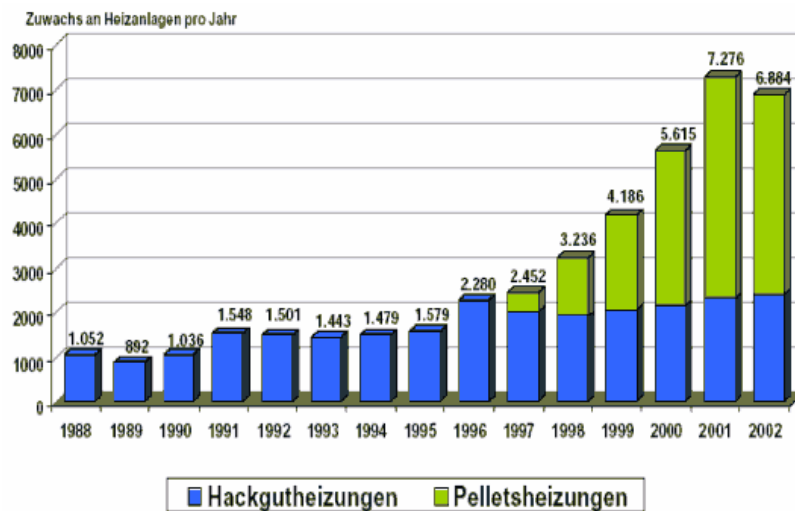
Biomass



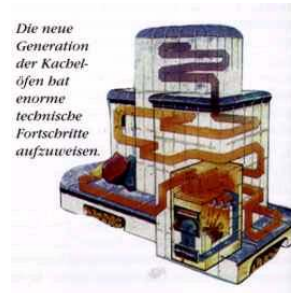
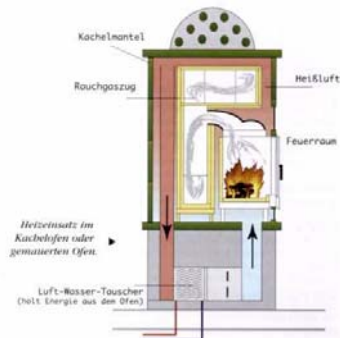
Jährlicher Leistungszuwachs bei Hackschnitzelanlagen
(1998 - 2002)



Yearly increase of biomass heating systems in Austria



„Kachelofen“



- Positioning that several rooms can be heated, with water HX inside a coupling to a water heating system can be done
- Efficiency about 60-70 %
- High startup emissions (cold burning chamber)

„Kaminofen“



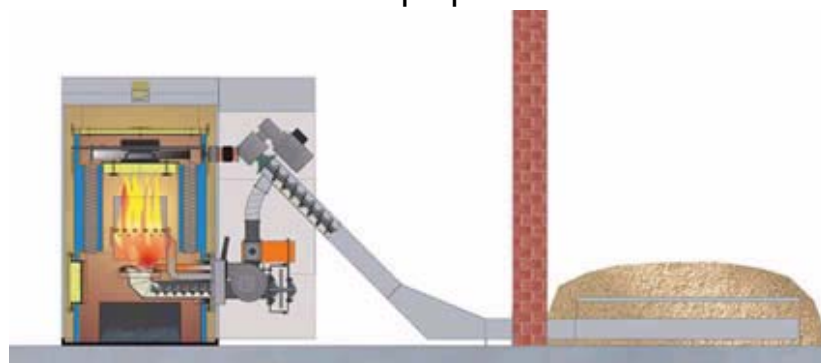
- Positioning that several rooms can be heated, with water HX inside a coupling to a water heating system can be done
- Efficiency about 60-70 %
- High startup emissions (cold burning chamber)

Log wood burner with downward flame



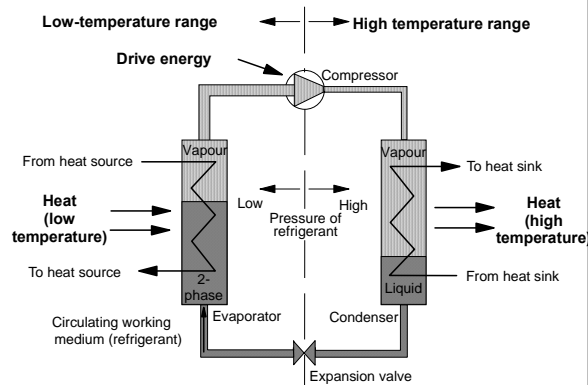
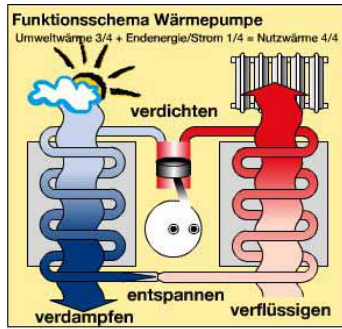
- Logs and ash is transported automatically downwards
- Logs are dried before burned
- Burning chamber is NOT cooled

Automatic wood chips/pellets burner

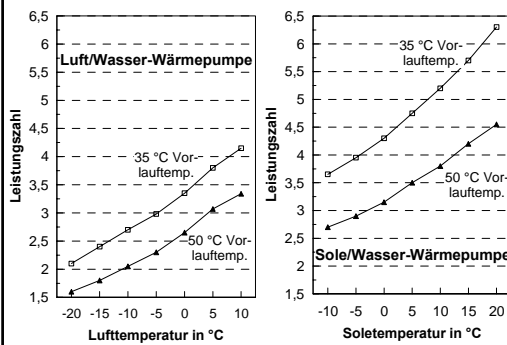


- Similar maintenance a soil or gas burners
- Similar emissions as oil burner
- Slightly higher investment than oil burner
- Biomass store has to be reached by the blowing tube of the truck

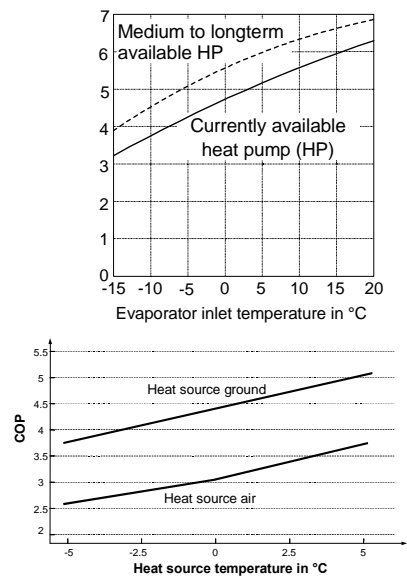
Heat pumps



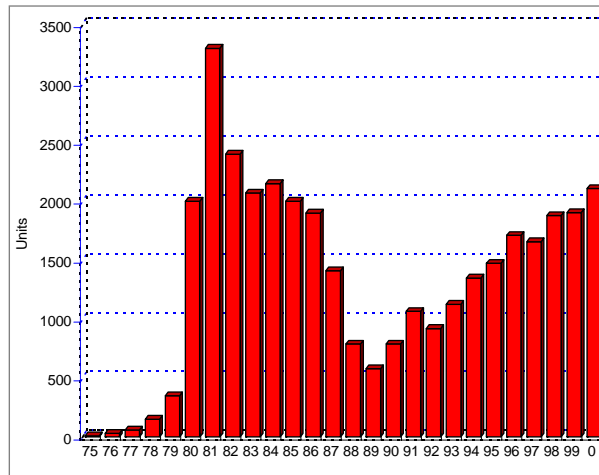
Heat pump COP and boundary conditions



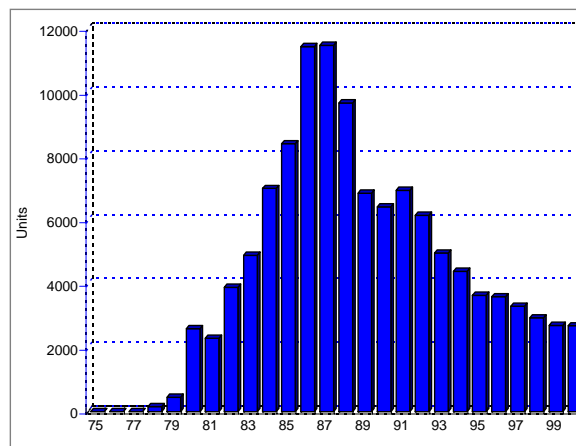
Quelle: Kaltschmitt, Streicher, Wiese, 2006



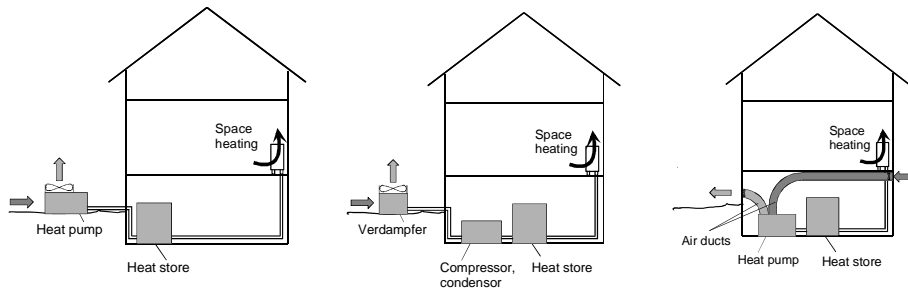
Space heating heat pumps in Austria



Domestic hot water heat pumps in Austria



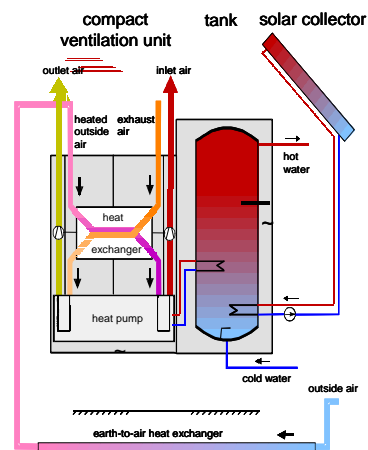
Ambient air as heat source



Quelle: Kaltschmitt, Streicher, Wiese, 2006

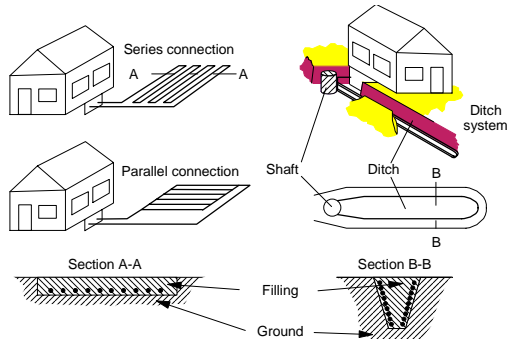
Compact heating and domestic hot water unit

- air-to-air heat recovery
- exhaust air heat pump
- storage
- solar collector
- earth-to-air heat exchanger



Source: Fraunhofer-Institut für Solare Energiesysteme ISE, 2000

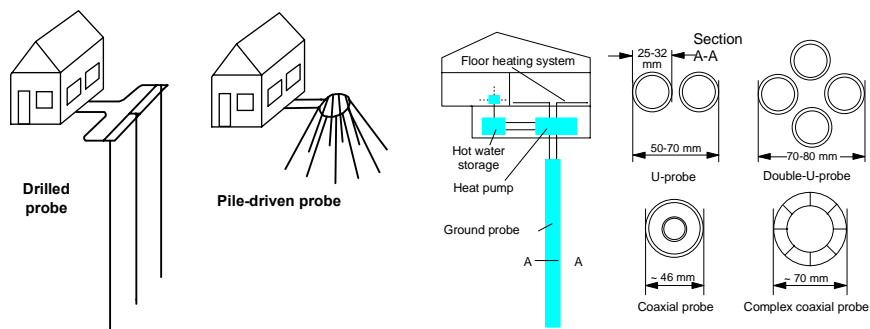
Ground as heat source



Type of soil	Withdrawn heat capacity
Dry, sandy soil	10 – 15 W/m ²
Humid, sandy soil	15 – 20 W/m ²
Dry loamy soil	20 – 25 W/m ²
Humid loamy soil	25 – 30 W/m ²
Water saturated sand/gravel	30 – 40 W/m ²

Quelle: Kaltschmitt, Streicher, Wiese, 2006, VDI 4640

Ground as heat source



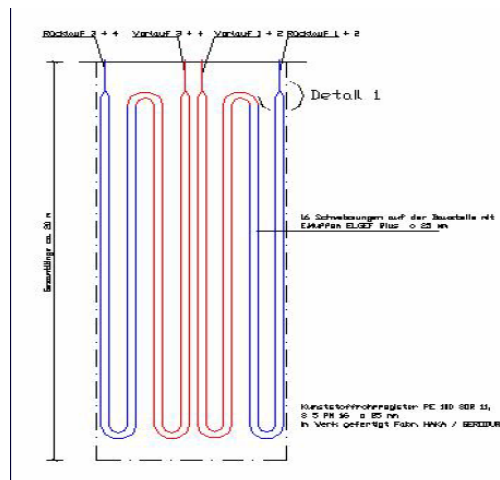
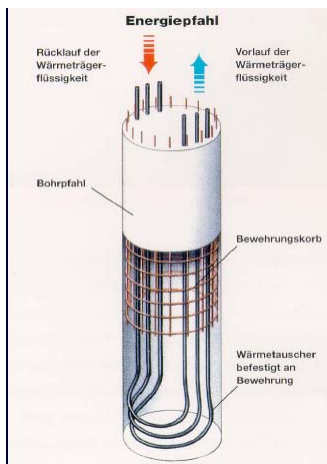
Quelle: Kaltschmitt, Streicher, Wiese, 2006

	1 800 h/a	2 400 h/a
General guidelines		
Bad subsoil (dry lose rocks)	25 W/m	20 W/m
Solid rock subsoil, water-saturated lose rock	60 W/m	50 W/m
Solid rock with high heat conductivity	84 W/m	70 W/m
Individual soils		
Gravel, sand, dry	< 25 W/m	< 20 W/m
Gravel, sand, carrying water	65 – 80 W/m	55 – 65 W/m
Gravel, sand, strong groundwater flow, for small systems.	80 – 100 W/m	80 – 100 W/m
Clay, loam, moist	35 – 50 W/m	30 – 40 W/m
Limestone (solid)	55 – 70 W/m	45 – 60 W/m
Sandstone	65 – 80 W/m	55 – 65 W/m
Acidic magmatites (e. g. granite)	65 – 85 W/m	55 – 70 W/m
Alkaline magmatites (e. g. basalt)	40 – 65 W/m	35 – 55 W/m
Gneiss	70 – 85 W/m	60 – 70 W/m

The requirement for using the table: only heat withdrawal (heating incl. hot water) takes place; length of the individual ground probes between 40 and 100 m; smallest space between two ground probes would be a minimum of 5 m for ground probe lengths of 40 to 50 m or at least 6 m for ground probes with lengths of over 50 to 100 m. Suitable ground probes are double-U probes with an individual tube diameter of 25 or 32 mm or coaxial probes with at least a diameter of 60 mm. The values given above can fluctuate considerably, depending on rock formations such as crevasses, foliation and weathering.

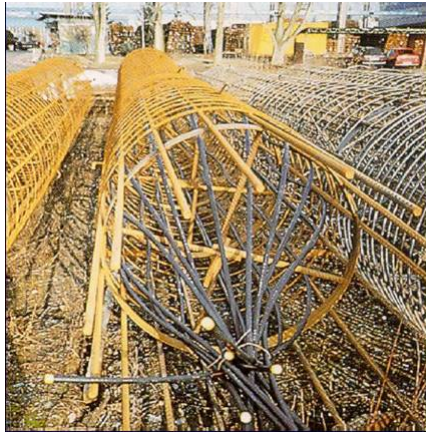
Quelle: Kaltschmitt, Streicher, Wiese, 2006, VDI 4640

Energy poles



Quelle: Sauerwein, Bilfinger Berger,

Vorgefertigter Bewehrungskorb



Energy poles

Verteilerstation Energiepfähle

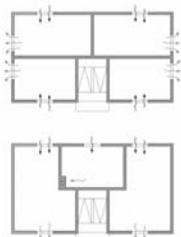


Natural ventilation

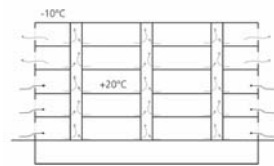
Natürliche Luftströmung durch Gebäude



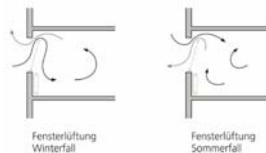
Querlüftung bei natürlicher Lüftung



Schachtwirkung durch thermischen Auftrieb



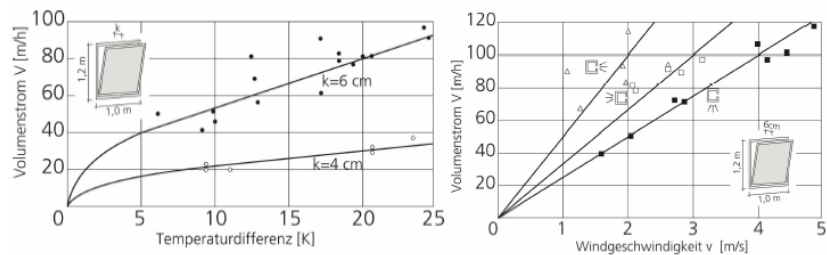
Natürliche Lüftung Sommer/Winter



Quelle: Bohne, Skript techn. Gebäudeausrüstung, UNI-Hannover

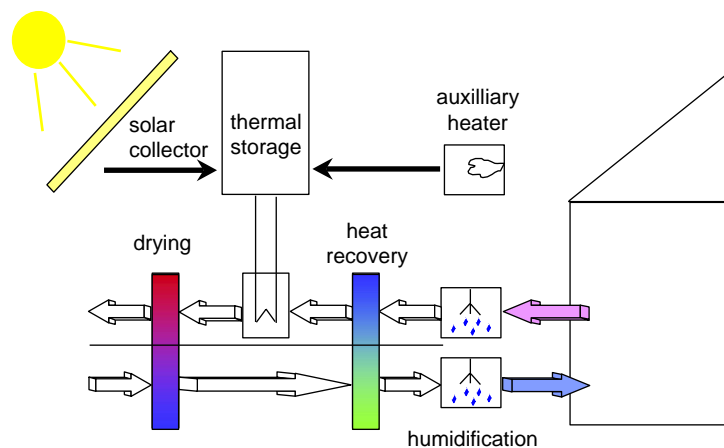
Natural ventilation

Luftaustausch bei natürlicher Lüftung durch Temperaturdifferenz und Windgeschwindigkeit

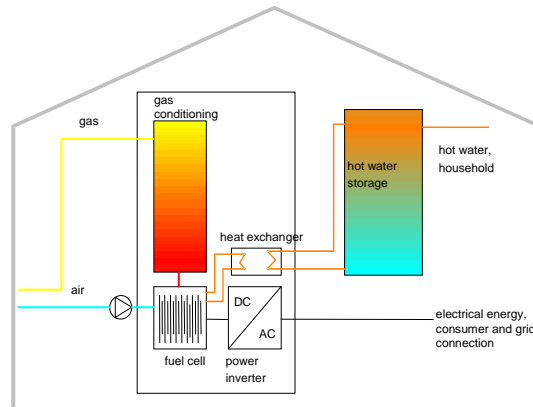


Quelle: Bohne, Skript techn.
Gebäudeausrüstung, UNI-Hannover

Solar desiccant cooling



Domestic fuel cell system



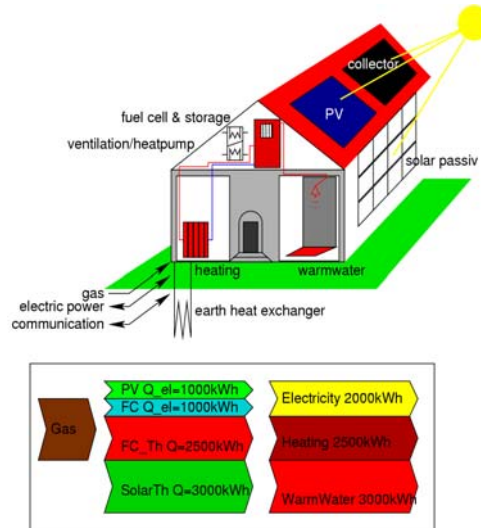
New control strategies

Higher efficiency

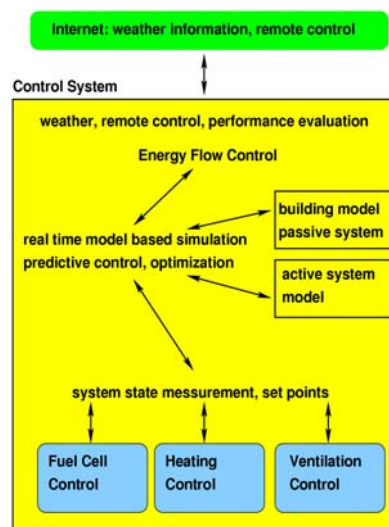
Total energy supply concepts

Integration into the grids

Concept of the domestic supply with fuel cells



Control strategy



Summary

New materials enable new systems

New systems enable new energy concepts for buildings

New control strategies enable an optimized energy supply

Always under consideration of comfort and health, cost and economy and available resources